

**Figure 3-2 Section of Segment of Shield Tank End Wall used to Compare Edge Fixing Concepts**

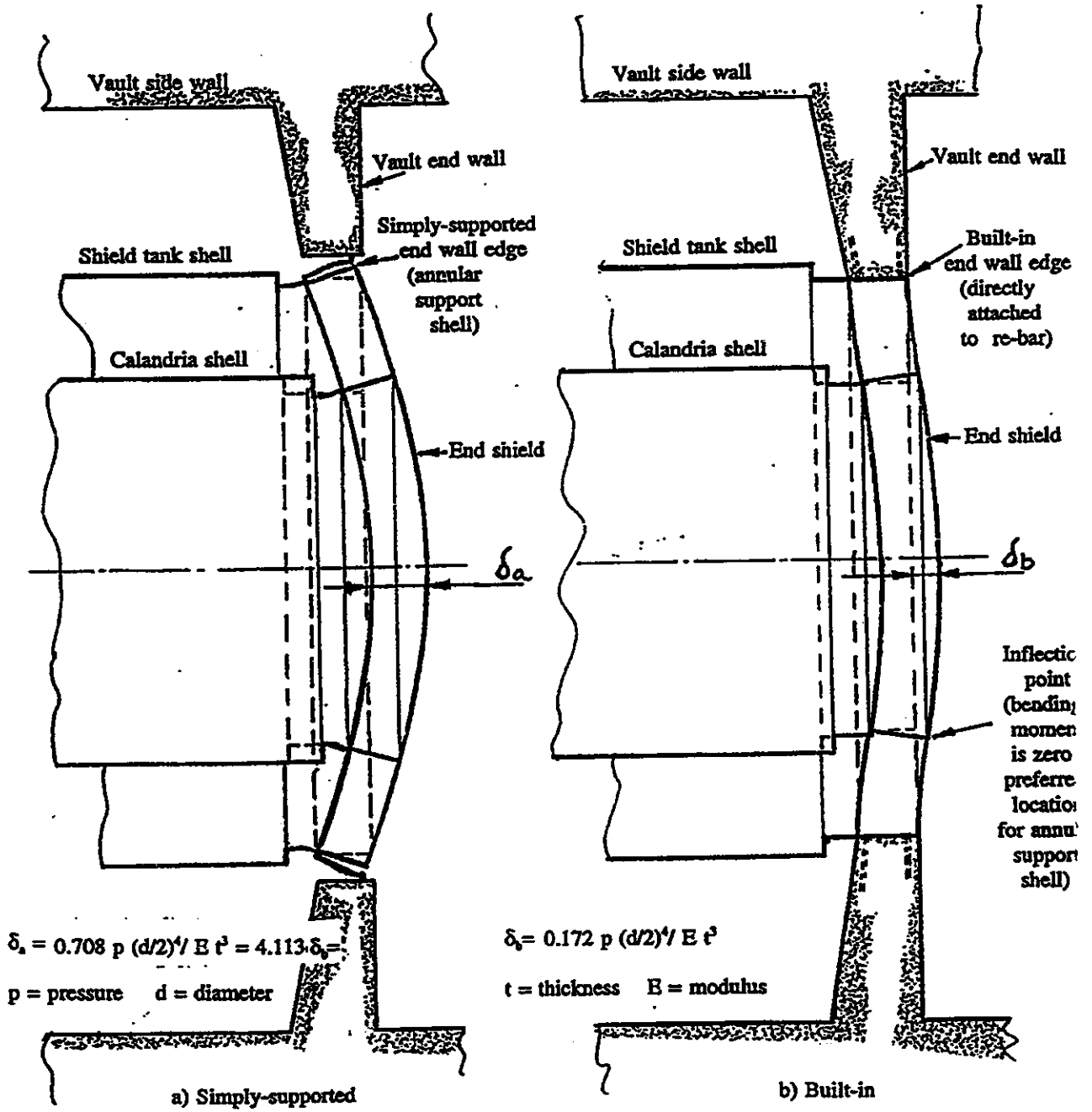
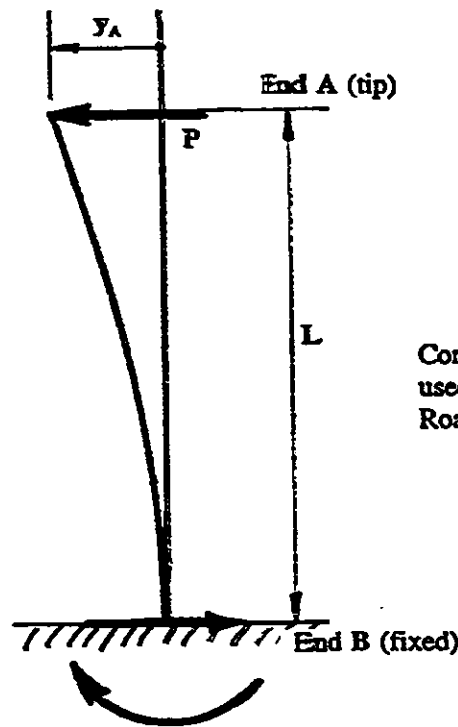
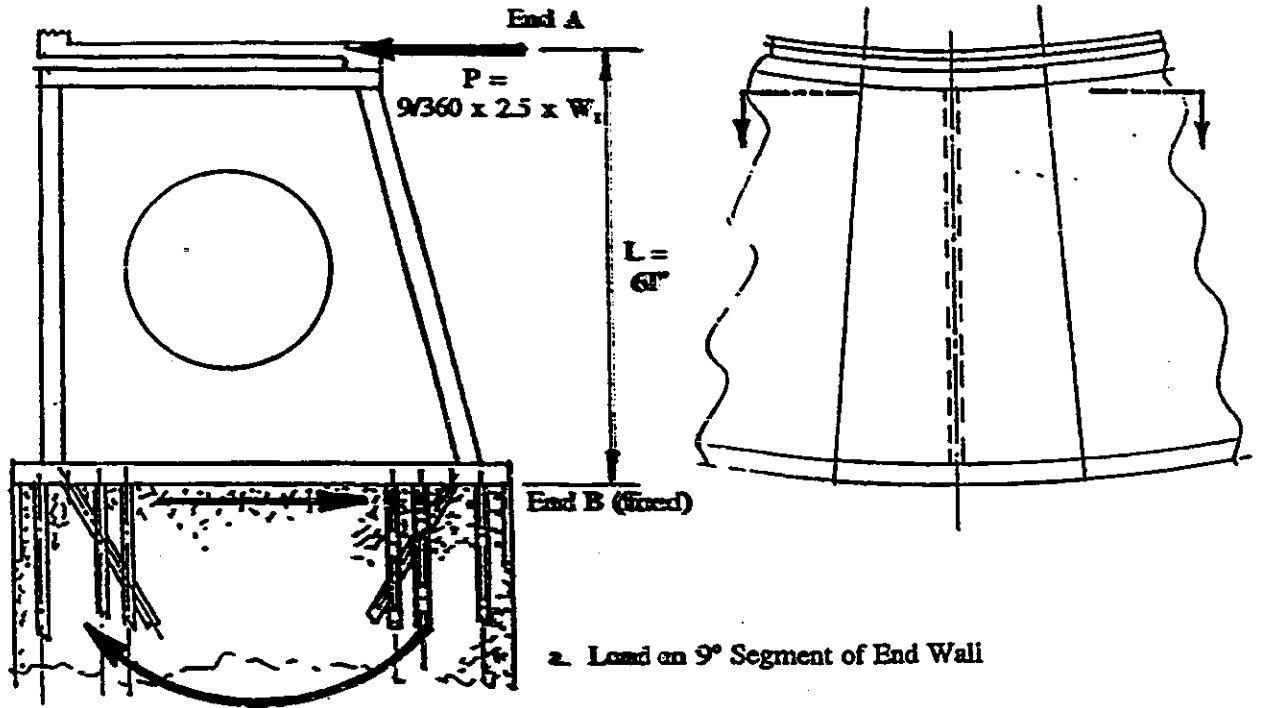


Figure 3-3 Comparison of Deflected Shapes and Magnitude for Simply-Supported and Built-In Flat Plates



Convention of parameter identification used in Tapered Beam Equations in Roark, Table 13d, Case Ia, for  $a=0$ .

b. Convention of parameter identification

Figure 3-4 Deflections and Stiffness of Built-In End Wall Design

SUMMARY OF  
DIFFERENCES IN DESIGN

- BY RULE
- BY ANALYSIS

- MATERIALS
- MANUFACTURING
- INSPECTION
- STRESS LIMITS

BY RULE - 3100	BY ANALYSIS - 3200
<ul style="list-style-type: none"> <li>- BASED ON MAXIMUM STRESS VALUE</li> <li>- <math>S_A</math>: HIGHER FACTOR OF SAFETY 5/8 Y.S. OR 1/4 UTS</li> <li>- SIMPLE ANALYSIS</li> <li>- SIMPLE SERVICE CONDITIONS</li> <li>- LIMITED DESIGN CONFIGURATIONS</li> </ul>	<ul style="list-style-type: none"> <li>- BASED ON MAXIMUM STRESS INTENSITY</li> <li>- <math>S_M</math>: LOWER FACTOR OF SAFETY- MIN. OF 2/3 Y.S. OR 1/3 UTS</li> <li>- DETAILED ANALYSIS</li> <li>- SEVERE OPERATING CONDITIONS</li> <li>- NO LIMIT ON DESIGN CONFIGURATIONS</li> </ul>

Figure 3-5 Allowable Stresses for Design-by-Rule & Design-by-Analysis Methods

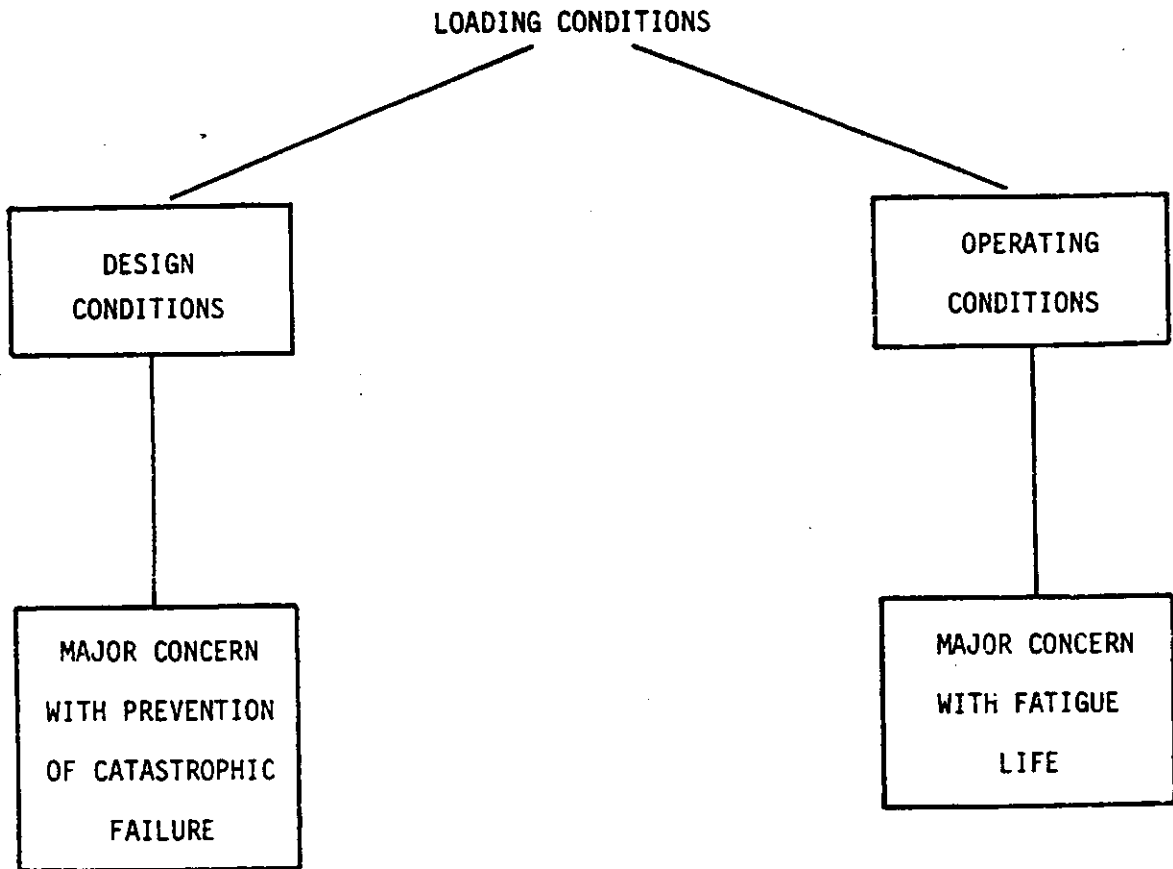


Figure 3-6 Two Main Categories of Loading Conditions

OPERATING CONDITIONS

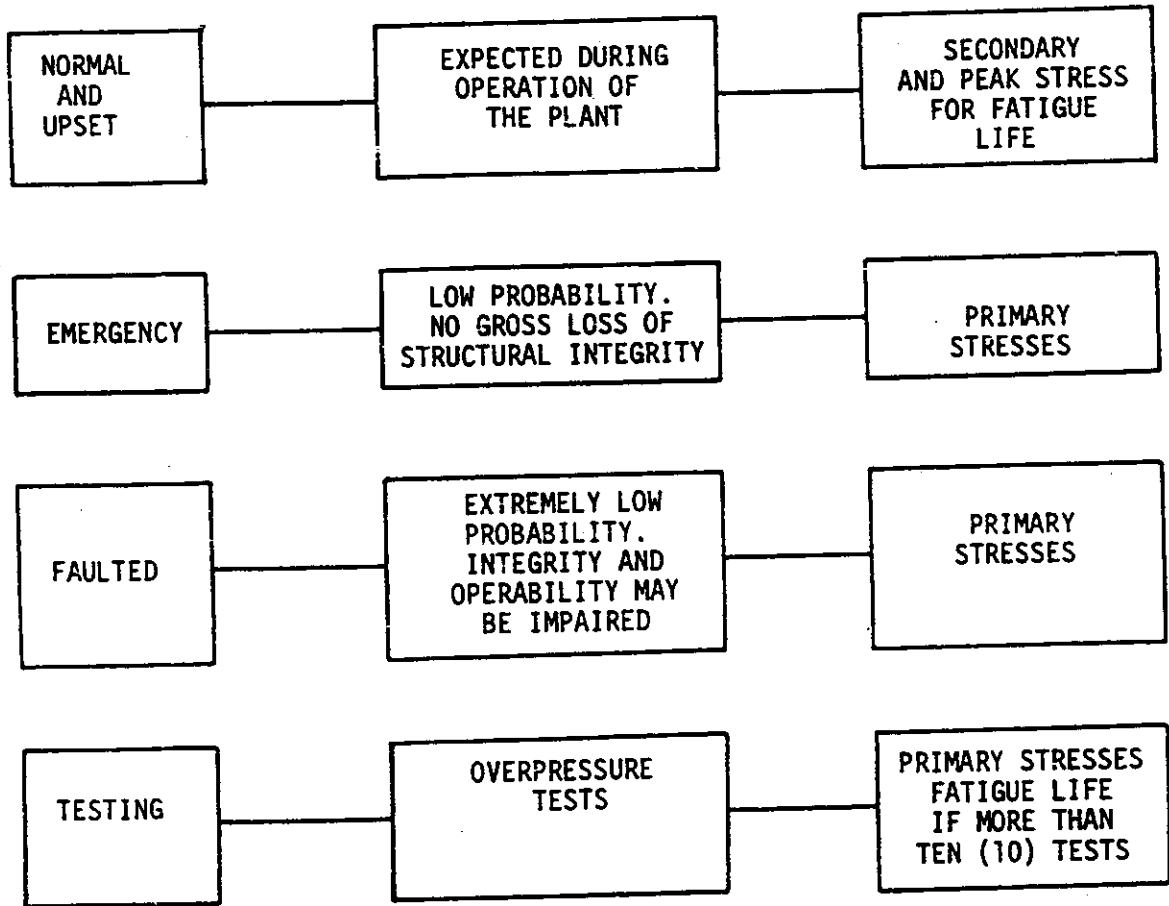


Figure 3-7 Operating Conditions

## OPERATING OR SERVICE LEVELS

### NORMAL OPERATION SERVICE LEVEL A AND B

SERVICE LEVEL 'A' AND 'B' LIMITS ARE PROVIDED TO EVALUATE COMPONENT STRESSES AND EFFECT OF SYSTEM OPERATING LOADS ON THE FATIGUE LIFE OF THE COMPONENT (FIGURE 6).

### SERVICE LEVEL C OR EMERGENCY

THESE LEVELS ARE PROVIDED IN ORDER TO EVALUATE THE EFFECT OF PLANT OPERATING LOADS ON THE STRUCTURAL INTEGRITY OF A COMPONENT FOR SITUATIONS WHICH ARE NOT ANTICIPATED TO OCCUR FOR A SUFFICIENT NUMBER OF TIMES TO AFFECT THE FATIGUE LIFE AND FOR WHICH LARGE DEFORMATIONS IN THE AREA OF DISCONTINUITIES ARE NOT OBJECTIONABLE. UNDER THIS CONDITION REACTOR IS SHUT DOWN AND THE VARIOUS COMPONENTS ARE INSPECTED FOR DAMAGE AND THE COMPONENTS MAY BE REMOVED FOR REPAIRS

### SERVICE LEVEL D OR FAULTED CONDITION

THIS LIMIT IS PROVIDED IN ORDER TO EVALUATE THE EFFECT OF PLANT OPERATING LOADS ON THE STRUCTURAL INTEGRITY OF A COMPONENT FOR SITUATIONS IN WHICH GROSS GENERAL DEFORMATIONS, LOSS OF DIMENSIONAL STABILITY AND DAMAGE REQUIRING REPAIR, EXCLUDING LOSS OF PRESSURE RETAINING FUNCTION ARE NOT OBJECTIONABLE.

REQUIRES SAFE SHUTDOWN. REACTOR AND COMPONENTS MAY BE A WRITE OFF.

### DESIGN AND TEST LOADS

SPECIAL LIMITS APPLY TO DESIGN AND TEST LOADS. BUT ONE CAN CONSERVATIVELY CHOOSE TO APPLY SERVICE LEVEL 'A' LIMITS FOR THE DESIGN AND TEST LOADS.



SUMMARY OF OPERATING CONDITIONS  
IN OLD AND NEW CODE

<u>PRE 1974 CODE</u>	<u>POST 1974 CODE</u>
<u>LOADING CONDITION</u>	<u>SERVICE LEVEL</u>
DESIGN CONDITION	CONSERVATIVELY WE CHOOSE TO APPLY LEVEL A
NORMAL OPERATION	LEVEL A OR LEVEL B
UPSET CONDITIONS	LEVEL B
EMERGENCY CONDITION	LEVEL C
FAULTED CONDITION	LEVEL D
TEST CONDITIONS	CONSERVATIVELY WE CHOOSE TO APPLY LEVEL A

**Figure 3-9 Service Level Category Definitions before and after 1974**

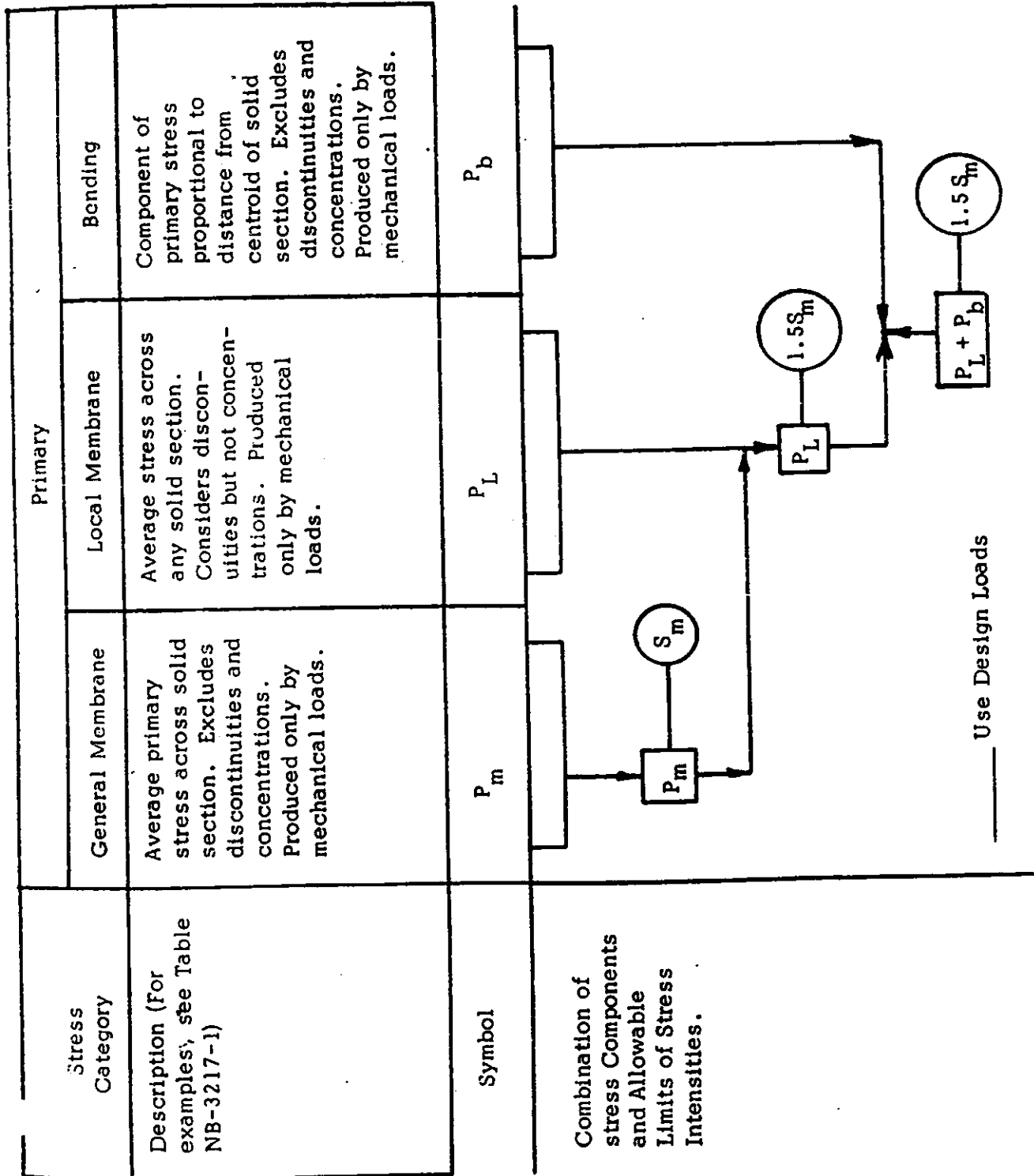


Figure 3-10 Allowable Stress Intensities for Design Condition

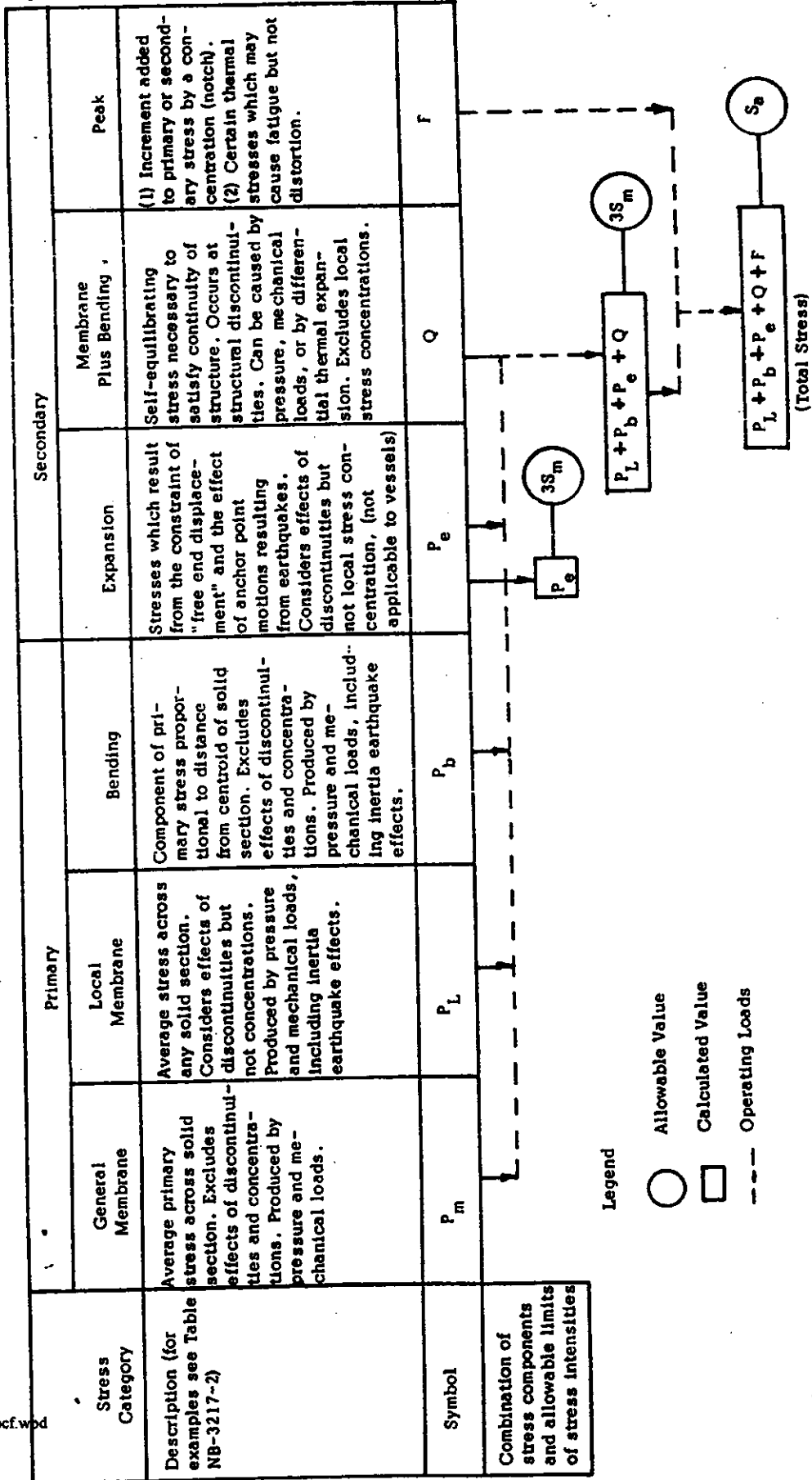


Figure 3-11 Allowable Stress Intensities for Normal & Upset Operating Conditions

Stress Category	Primary Stresses (Notes 1 & 4)			Secondary Stresses (Note 1)	Peak Stresses (Note 1)
	General Membrane	Local Membrane	Bending		
Description (For examples see Table NB-3217-1)	Average primary stress across solid section. Excludes discontinuities and concentrations. Produced only by mechanical loads.	Average stress across any solid section. Considers discontinuities but not concentrations. Produced only by mechanical loads.	Component of primary stress proportional to distance from centroid of solid section. Excludes discontinuities and concentrations. Produced only by mechanical loads.	Self-equilibrating stress necessary to satisfy continuity of structure. Occurs at structural discontinuities. Can be caused by mechanical load or by differential thermal expansion. Excludes local stress concentration.	(1) Increment added to primary or secondary stress by a concentration (Notch) (2) Certain thermal stresses which may cause fatigue but not distortion of vessel shape.
Symbol (Note 1)	$P_m$ NB-3213.6 & .8 (Note 5)	$P_L$ NB-3213.10	$P_b$ NB-3213.7 & .8	$Q$ NB-3213.9	$F$ NB-3213.11
For Level C Service Limits					
Combination of Stress Components and Allowable Limits of Stress Intensities					

NOTES:

- The symbols  $P_m$ ,  $P_L$ ,  $P_b$ ,  $Q$ , and  $F$  do not represent single quantities, but rather sets of six quantities representing the six stress components  $\sigma_x$ ,  $\sigma_y$ ,  $\sigma_z$ ,  $\tau_{xy}$ ,  $\tau_{yz}$ , and  $\tau_{zx}$ . The collapse load calculated on the basis of the lower bound theorem of limit analysis and yield strength values specified in Table 1-2.1 or 1-2.2 (NB-3213.22).
- $CL$  the collapse load calculated on the basis of the lower bound theorem of limit analysis and yield strength values specified in Table 1-2.1 or 1-2.2 (NB-3213.22).
- The triaxial stresses represent the algebraic sum of the three primary principal stresses ( $\sigma_1 + \sigma_2 + \sigma_3$ ) for the combination of stress components.
- For configurations where compressive stresses occur, the stress limits shall be revised to take into account critical buckling stresses (NB-3211(c)).
- The limits shown are for stresses resulting from pressure in combination with other mechanical loads. For ferritic materials, the  $P_m$  elastic analysis limits for pressure loadings alone shall be equal to the greater of  $1.15P_m$  or  $0.9S_y$ . For the  $P_L$  and  $P_b$  limits, a factor of 1.5 shall be applied to the  $P_m$  limits.

Figure 3-12 Allowable Stress Intensities for Level C Conditions

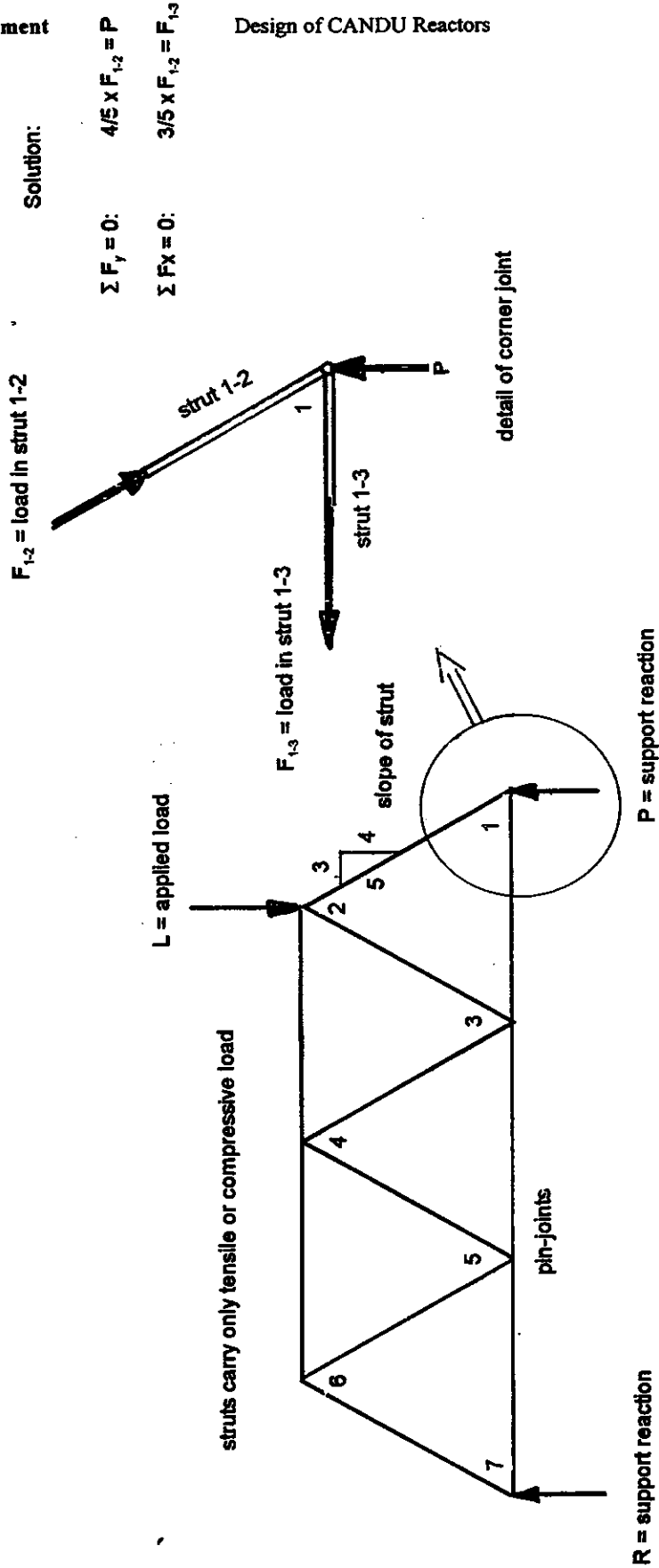
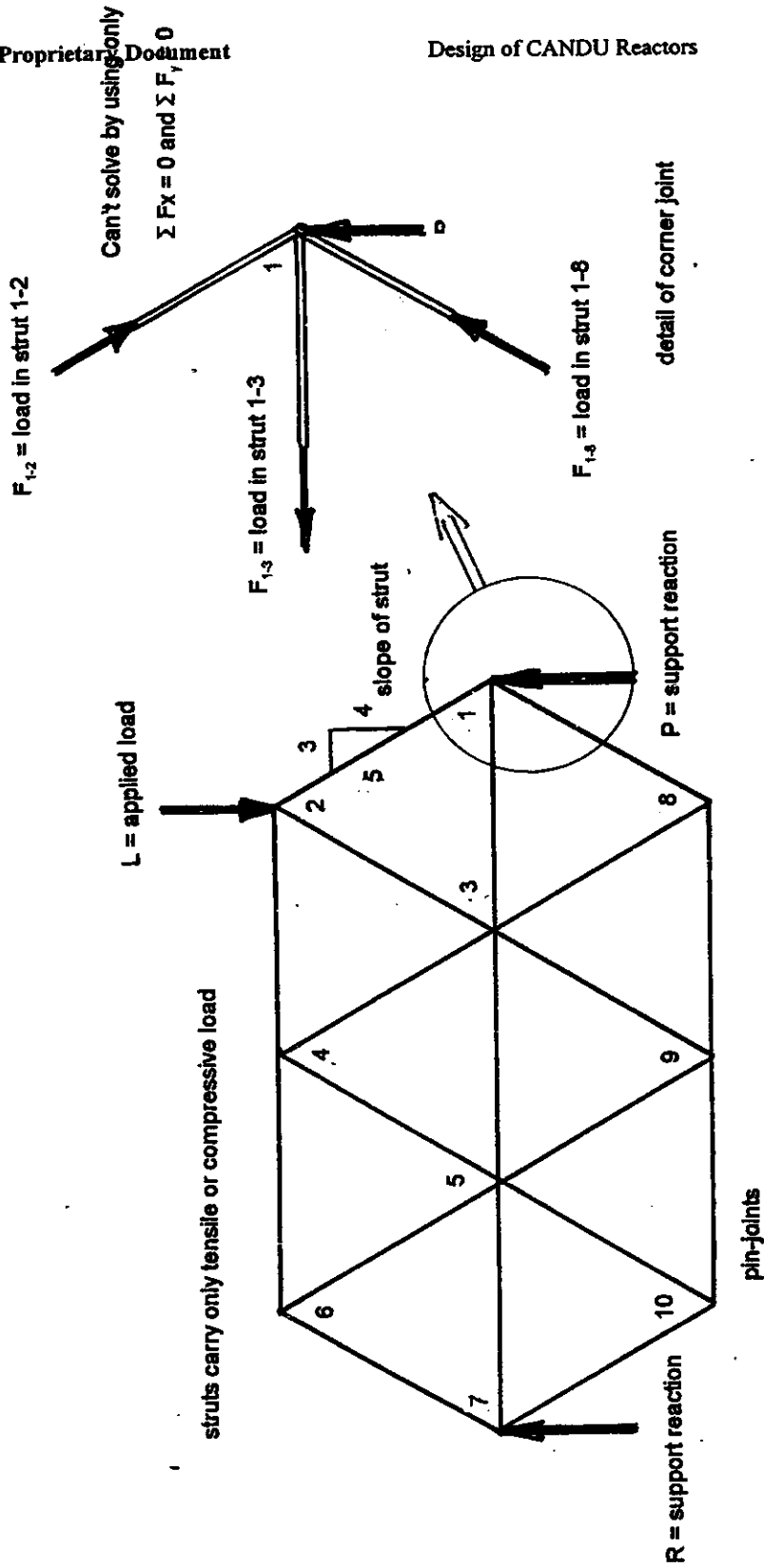


Figure 3-13 Simple Pin-Jointed Truss



Truss is redundant because any strut can be removed and truss will still carry load

Figure 3-14 Redundant Pin-Jointed Truss

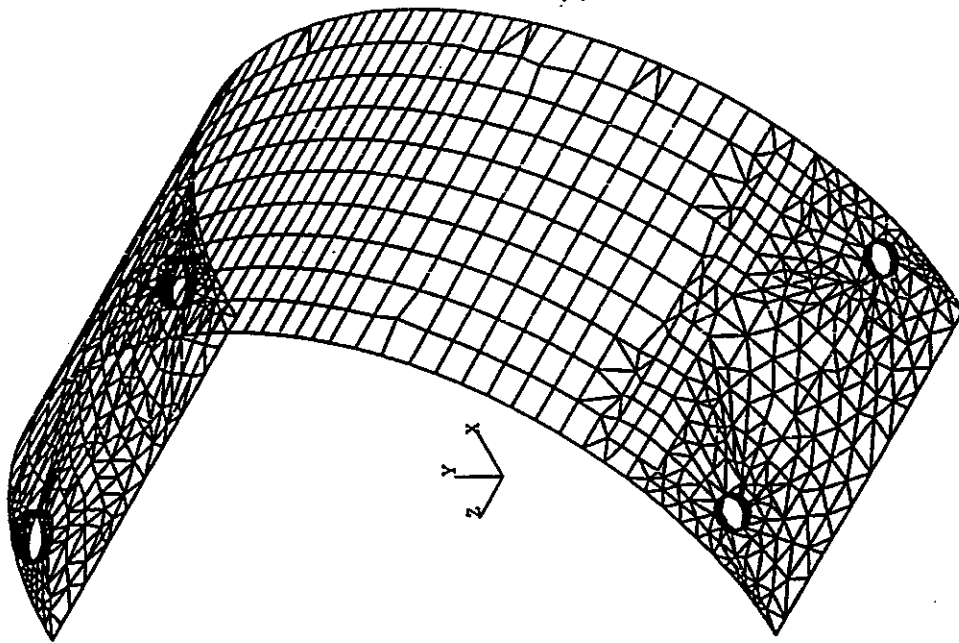


Figure 3-15 Finite Element Model for a CANDU Reactor Calandria Shell

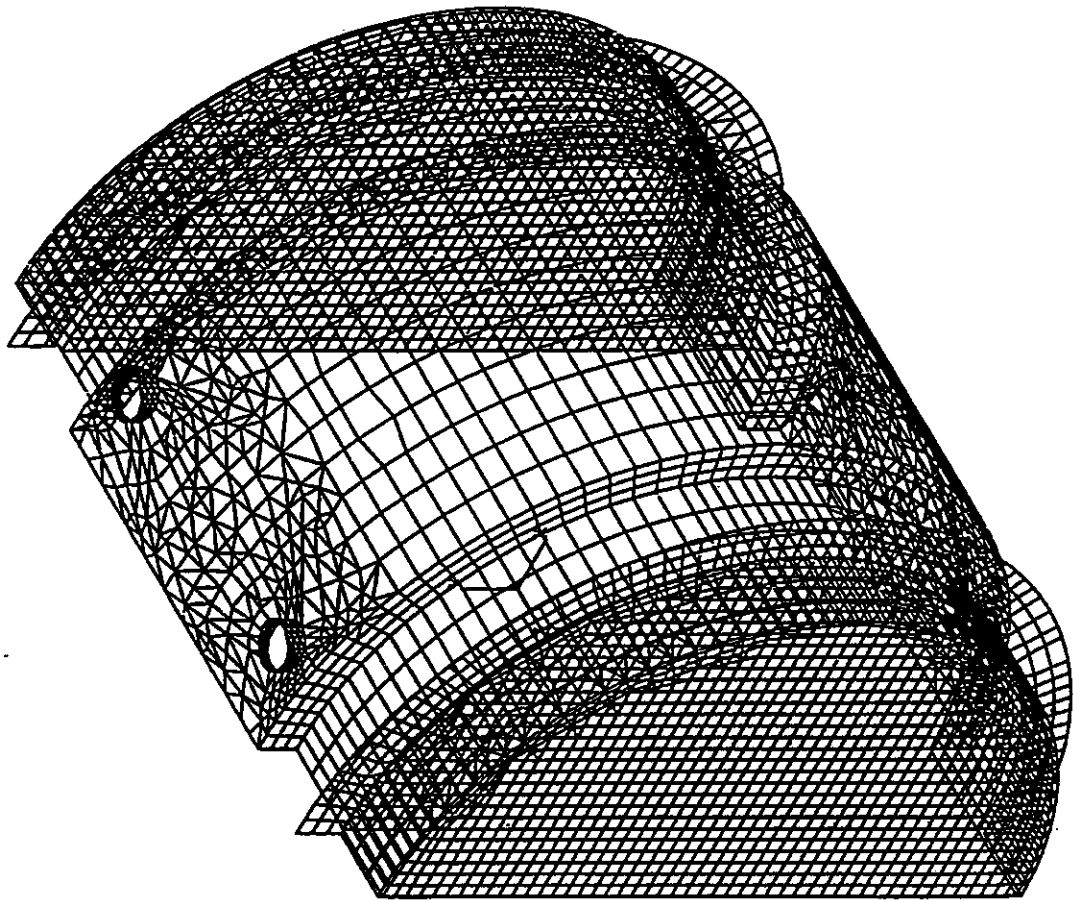


Figure 3-16 Finite Element Model for a CANDU Reactor Structure



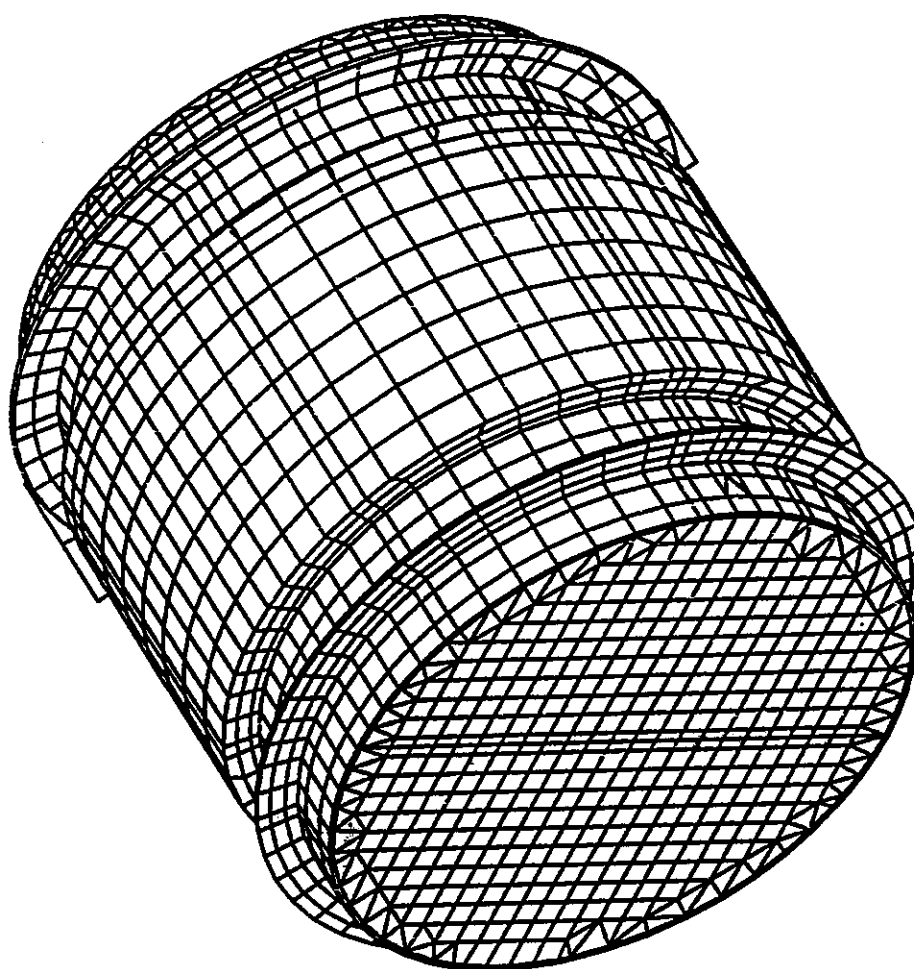
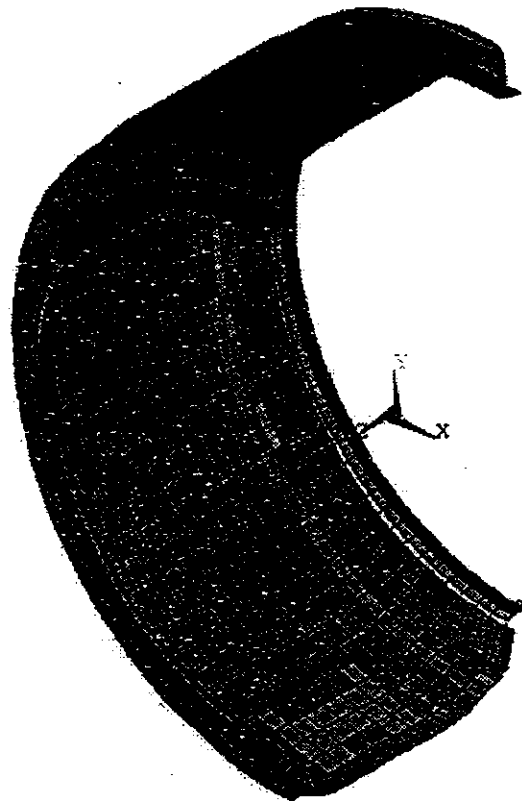
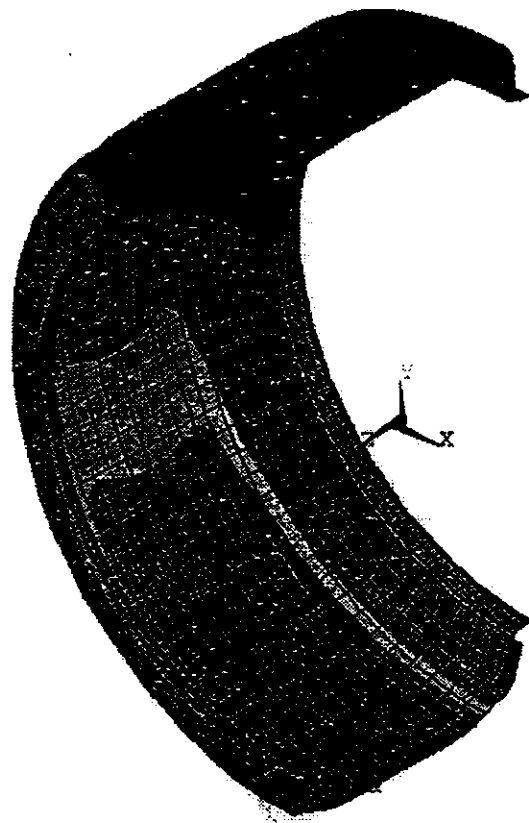


Figure 3-17 Seismic Finite Element Model for a CANDU Calandria  
Structure Assembly



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SMN =8522  
SMX =59974  
8522  
14239  
19955  
25672  
31389  
37106  
42823  
48540  
54257  
59974
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Figure 3-18 Graphical Display of Stresses for a CANDU Reactor Structure



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UX  
BOTTOM  
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DMX =2.206  
SEPC=26.321  
SMN =-.635465  
SMX =2.202  
- .635465  
- .320241  
- .005018  
.310205  
.625429  
.940652  
1.256  
1.571  
1.886  
2.202
```

Figure 3-19 Graphical Display of Deflections for a CANDU Reactor Structure